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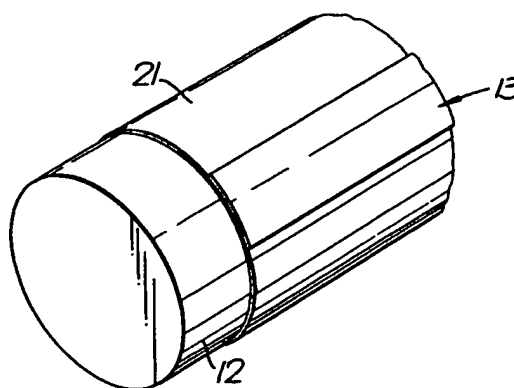
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⑤④ Arrangement and method for covering elongate substrates.

⑤⑦ An arrangement for covering at least part of an elongate object, for example a pipe, comprises a heat recoverable closure sheet 21 which can be wrapped around the substrate, a patch 13 and a layer of adhesive for securing the edge portions of the sheet together so that the sheet can be recovered about the substrate by the application of heat. Certain properties of the patch for example its modulus and elongation, and of the adhesive, for example its lap shear strength, are chosen so that at least part of the patch 13 will be stretched by at least 5% in the recovery direction of the sheet so that the sheet will not slip away from the patch when it is recovered.



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This invention relates to an arrangement for covering at least part of an elongate substrate which comprises a heat-recoverable polymeric closure member in sheet form adapted to be wrapped around the substrate so that one edge portion thereof overlies an opposite edge portion and recovered about the substrate by application of heat, a patch member for retaining the edge portions together during recovery of the closure member, and a layer of adhesive having a tack temperature below the recovery temperature of the closure member for retaining the patch member on the closure member.

Many methods of enclosing elongate substrates have been proposed, and reference may be made, for example, to U.S. Patents Nos. 3,379,218; 3,455,336; 3,530,898; 3,542,077; 3,574,313 and 3,770,556 and 4,200,676, the disclosures of which are incorporated by reference herein.

The present invention is characterized in that the layer of adhesive has a lap shear strength at 150°C of from 70 to 14,100 kg.m^{-2} (0.1 to 20 psi), preferably from 200 to 14,100 kg.m^{-2} (0.3 to 20 psi) and especially from 7000 to 8,500 kg.m^{-2} (1 to 12 psi), and the patch member has a modulus at 150°C of from 1,400 to 141,000 kg.m^{-2} (2 to 200 psi) preferably from 7000 to 141,000 kg.m^{-2} (10 to 200 psi), especially from 35,000 to 106,000 kg.m^{-2} (50 to 150 psi), and an elongation at 150°C of from 10 to 1000%, preferably from 50 to 200%, the arrangement being such that when the closure member is heated, it will recover about the

substrate and cause at least part of the patch member to stretch by at least 5%, preferably from 5 to 50% in the direction of recovery of the closure member.

The arrangement according to the present invention has a number of advantages as compared with the previously proposed closure systems, for example it is not necessary (as it is in U.S. Patent No. 3,770,556) for the edge portions of the closure member to be coated with a contact adhesive and so a single arrangement can be used to cover substrates of widely differing sizes. In addition it is possible to use a patch member in the present arrangement that is less bulky and complex than that used in the system described in U.S. Patent No. 4,200,676, so that the underlying adhesive can be heated more quickly and will, when the heat source is removed, cool and bond that patch member to the closure member, more quickly, thereby enabling the installer to move to a different section of the substrate without too great a delay. A further advantage of the arrangement according to the invention is that, in certain cases, it is possible to provide a covering for substrates of irregular diameter as in the case where a telephone or high-voltage cable transition or a joint between pipes of different diameter is to be covered. To accommodate such a transition the patch must be able to deform (i.e. stretch) in the areas of greatest stress to thereby more evenly distribute the recovery stress and avoid peeling of the patch away from the

closure member. The substantially undeformable patch described in the U.S. Patent No. 4,200,676 cannot stretch significantly and hence is subject to pulling away of the closure in regions of high recovery stress such as is caused by a major diametric transition. Likewise, a reinforced patch is unsuitable for substrates of small diameter since its comparative stiffness makes it difficult or impossible for the installer to position it on the closure member so that it will conform to the closure member.

The patch member used in the present invention is preferably of uniform cross-section and composition and preferably has the layer of adhesive initially adhered to it. The patch member is preferably composed of a polymeric material, which polymer will preferably be cross-linked, e.g. by irradiation, so that it retains strength even when it is heated above its crystalline melting point but can nevertheless stretch. However, other materials e.g. aluminium foil, can be used provided that they can stretch by at least 5% during installation. Reinforced patch members of the kind disclosed in U.S. Patent No. 4,200,676 do not, as indicated above, stretch sufficiently. It has been found that if the patch member cannot stretch circumferentially by at least about 5% at any point along its length, and thereby help to accommodate recovery of the closure member and reduce and more uniformly distribute the shear stress on the adhesive layer, the closure member can exert sufficient recovery force at

one or more points to slip away from underneath the patch and thereby expose the substrate. Such incomplete covering of the substrate by the closure member is, of course, totally unacceptable. Often at least a part of the patch should stretch by up to about 5% or even more. Preferably no part of the patch should stretch by more than about 50%. Stretching in excess of about 50% is undesirable as it permits the sheet closure to contract during recovery to such an extent that it may no longer overlap and will therefore not fully cover the substrate, i.e. it will leave only the patch itself over a longitudinal band of the substrate which is unacceptable.

When a substrate of varying cross-section is being covered, the patch may stretch only in the area of greatest circumference, and may not stretch at all (or may indeed contract) in other areas. Since the patch will preferably be capable of stretching by at least 5%, it is generally preferred that it should not be heat-shrinkable. However, since the forces generated by recovery of the closure member can overcome forces generated by any tendency of the patch to shrink on heating, it is possible for the patch to be heat-shrinkable; it can also be heat-expandable. Since the patch must secure the overlapped portions of the closure member together along substantially the whole length of the closure member overlap, it is preferred that any change in the axial length of the patch during installation should substantially match any change occurring in the axial length

of the closure member. Generally, this means that its axial length should remain substantially unchanged during installation. Bearing these points in mind it is preferred that the patch member comprise a polymeric material which, when heated in the absence of restraint, undergoes a maximum dimensional change in the axial and/or circumferential (i.e. longitudinal and/or transverse) direction of -10 to +10%, preferably substantially zero. Unrestrained dimensional changes in excess of $\pm 10\%$ are undesirable because if the patch undergoes such change when unrestrained, it tends to curl under along its periphery in use thereby inhibiting good adhesion to the underlying closure member and precluding effective sealing. The patch member preferably has a thickness in the range of from 0.25 to 2.54mm (10 to 100 mils), more preferably from 0.38 to 0.76mm (15 to 30 mils). The thickness of the patch member should preferably be less than the recovered thickness of the closure member and most preferably will be less than the thickness of the closure member before recovery.

It has been found that the relationship between the maximum recovery force of the closure member (i.e. the recovery force when shrinkage begins) and the product of the thickness and the hot modulus of the patch member has an important influence on successful operation of the method of the present invention. It is conjectured that this is at least in part because this relationship significantly affects the radial forces which press together the overlapping portions of the closure member. When at least



part of the interior surface of the first marginal portion and the exterior surface adjacent to the second marginal portion in contact therewith are free from any coating, the heating of the closure member, coupled with the radial component of the recovery forces, may cause melt-bonding of the first and second marginal portions which is particularly desirable in terms of achieving a secure closure. The product of the thickness of the patch member and its modulus at 150°C is preferably at least 0.36 times but not more than 20 times, more preferably between about 0.5 and 10.0 times and especially at least equal to, the maximum recovery force (per unit length) of the closure member, in order that the patch member be sufficiently compliant and extensible. In carrying out the method of the present invention, it is desirable that in the finished product, the first and second marginal portions of the closure member should remain in overlapping contact with each other throughout their length. Proper correlation of the hot modulus and thickness of the patch with the recovery force of the closure member has an important influence in obtaining this valuable result.

The patch member may have, on the interior surface thereof, one or more areas of pressure-sensitive adhesive which can serve to hold the patch in place until the hot melt adhesive reaches its tack temperature. However, the presence of such pressure-sensitive adhesive areas reduces the total strength of the ultimate bond between the patch and closure member, and other means are preferably employed to keep the patch in place.

The axial length of the patch member is generally determined by the length of the closure member and will preferably

be substantially equal to that of the closure member. Virtually any length of closure member can be successfully accommodated using the patch design of the present invention. The wider the patch, the more likely it is to secure together the overlapping portions of the closure member.

Typically the width of the patch will be from 5 to 25.4cm (2 to 10 inches). With substrates of small circumference, especially when the substrate is of irregular cross-section, the maximum width for the patch will be influenced by the circumference of the substrate, the shrinkage of the closure member and the slippage on recovery (if any) of the marginal portions of the closure member relative to the patch. For this reason, the increased efficiency of the patch member of the present invention, as compared to those previously taught, is particularly valuable when the substrate to be covered is of small circumference, e.g. no greater than about 51cm (20 inches), especially at most 38cm (15 inches), and/or of irregular cross-section, e.g. the ratio of the maximum circumference to the minimum circumference is greater than about 2:1. Likewise, when substrates of large diameter (i.e. greater than 40cm or 16 inches) are to be covered the improved efficiency of the present patch design is a major advantage in that its narrow width in comparison with prior art designs enables rapid heating and installation and reduced material cost.

The adhesive preferably has a tack temperature below 140°C. Preferably it has a melt viscosity at 150°C of at least 10^2 poise, more preferably at least 10^4 poise, and preferably has a peel strength of at least 90 kg.m^{-1} (5 pli). The adhesive may be a hot-melt adhesive or, preferably a hot-melt adhesive that has been lightly cross-linked

and has a gel content of at least 1%, especially at least 5%. Hot-melt or modified hot-melt adhesives have the advantage of higher peel strengths as compared with contact adhesives, and so in contrast with the system described in U.S. Patent No. 3,770,556, allow a patch to be used in cases where the closure would be subject to significant peel forces. As adhesives that may be used in the arrangement according to the invention, certain adhesives described in U.S. Patent No. 4,200,676 and German Offenlegungsschrift No. 2,723,116 are suitable provided they satisfy the minimum requirements (e.g. lap shear strength) mentioned above. The adhesive layer advantageously has a thickness of from 0.12 to 2.54mm (5 to 100 mils). The preferred thickness is 0.25 to 0.51mm (10 to 20 mils) although in some cases slightly thicker layers, e.g. from 0.38 to 0.76mm (15 to 30 mils) may be used.

The sheet closure member may be any of the heat-shrinkable polymeric closure members of the type generally known to the prior art which provide a suitable surface for the patch member to adhere to. The present invention encompasses the use of sheet closure members formed by two or more sheet members joined to each other along axially extending bond lines, with at least one of the joints being formed between marginal portions from different closure members by means of a patch member in accordance with the present invention. Good results can be obtained when at least part of the closure member is not heat-recoverable. However, a drawback of a closure member of this kind is that it would be suitable for use only with substrates of a comparatively limited range of circumferential sizes, whereas the preferred procedure in most circumstances is to make use of a

uniformly expanded sheet of cross-linked polymeric material such as polyethylene which can be utilized to fit round any size of substrate by merely varying the degree of overlap, which is conveniently from 2.54 to 25.4cm (1 to 10 inches) The closure member will normally be from 0.254 to 3.81mm (10 to 150 mils) thick and have a circumferential expansion ratio of 1.05 to 10, preferably from 1.1 to 10, especially from 1.5 to 5, and a modulus at 150°C of from 1400 to 141,000 kgm^{-2} (2 to 200 psi), preferably from 20,000 to 42,000 kg.m^{-2} (30 to 60 psi), Preferably the closure member is uniaxially expanded in the direction transverse to the longitudinal axis of the substrate. The recovery force of the closure member will usually be from 1.8 to 360 kg.m^{-2} (0.1 to 20 pli), preferably from 18 to 180 kg.m^{-1} (1 to 10 pli). It is usually desirable for the closure member to have a coating of an adhesive (preferably a hot-melt adhesive) or mastic on the interior surface of the closure member which interior surface is moved into contact with the substrate when the closure member shrinks. As noted above, the best closure often results when at least part of the interior surface of the first marginal portion which overlaps the exterior surface of the second marginal portion is free from any such coating. However, completely satisfactory results can often be obtained even when the coating of adhesive or mastic covers the whole of the overlap area.

When bonding the patch member to the closure member, the patch will normally be heated to a temperature of about 80 to 300°C, generally 110-150°C.

According to another aspect, the invention provides a method

of covering at least part of an elongate substrate by means of an arrangement according to the invention, which comprises wrapping the closure member around the substrate so that one edge portion of the closure member overlies an opposite edge portion of the closure member, heating the adhesive to its tack temperature, placing the patch member and the layer of adhesive over the exposed edge and outwardly disposed edge portions of the closure member so that the layer of adhesive is interposed between the closure member and patch member, pressing the patch member against the closure member to bond them together, and heating the closure member to cause it to recover into circumferential contact with the substrate, the method being conducted under conditions such that the patch member remains bonded to the closure member over at least a major portion of its length and at least part of the patch member is stretched by at least 5% in the direction of recovery of the closure member.

One arrangement according to the invention and a method for its installation will now be described by way of example, with reference to the accompanying drawings in which:

Figure 1 is a perspective view of a closure member installed in accordance with the present invention;

Figure 2 is a view in cross-section of a patch member used in the present invention;

Figure 3 is a view in cross-section of a mastic or adhesive coated heat-recoverable closure member useful in the present invention;

Figures 4, 5 and 6 illustrate the method of the present invention by which the ends of a closure member are joined; and

Figure 7 illustrates a pipe system containing a transition which can be covered by the arrangement of the present invention.

Referring to the accompanying drawings, Figure 1 shows a pipe 12 having a closure member 21 recovered about it, with the ends of the closure member secured together by patch member 13. As shown in Figure 2, the patch member 13 comprises a cross-linked polymeric sheet 14 having a layer 15 of hot-melt adhesive adherent thereto, with marginal portions 16 and 17 of pressure-sensitive adhesive. Figure 3 is a cross-sectional view of the closure member prior to installation, showing cross-linked heat-shrinkable polymeric sheet 22 having adherent thereto a layer 23 of adhesive or mastic.

Figures 4, 5 and 6 illustrate the method of the present invention. As shown in Figure 4, the closure member 21 is wrapped around the substrate 12 with the marginal

portions 23 and 25 overlapping. Then patch 13 is approximately centered over the line formed by the exposed end 23, as shown in Figure 5. When in place, the panel 13 is heated, for example, by means of a torch 26 as shown in

Figure 6 or by other suitable heating means, to render the adhesive 15 tacky and is then pressed into firm contact with the closure member 21. Finally the exposed exterior surface of the closure member is heated to cause recovery thereof. Figure 7 illustrates a typical transition in a pipe system of the kind referred to in the Examples below in which a pipe 27,29 is surrounded at one point with a collar 28 of greater external diameter.

The following Examples, in which all percentages are by weight, illustrate the invention. The term length connotes the dimension of the patch or closure member which is parallel to the longitudinal axis of the substrate when applied while width is the dimension transverse to the substrate longitudinal axis. Both the patch and the closure member are ordinarily extruded in sheet form with the width of the sheet as extruded being the length of the patch or closure when applied to the substrate. Closure members in accordance with the present invention would ordinarily be supplied in rolls from which the installer would cut off the desired length to obtain a closure suitable for the diameter of the substrate.

Example 1

The patch member used in this Example is 45.7cm (18 inches) long and 15.24cm (6 inches) wide and consists of a 0.508mm (20 mil) thick sheet of cross-linked high density polyethylene having a modulus at 150°C of 77,330 kg.m⁻² (110 psi) and having adherent to one surface thereof a layer 0.635mm (25 mils) thick of a lightly cross-linked hot melt adhesive. The patch member is made by coating, onto a sheet of high density polyethylene which has been cross-linked by irradiation to a modulus at 150°C of 24,600 (35 psi), a layer of an adhesive composition comprising 72.82% of an ethylene/ethyl acrylate copolymer containing about 20% of ethyl acrylate (DPD 6181) 24.27% of a tackifier (Nevpene 9500), 1.94% of an antioxidant (Irganox 1010-tetrakis [methylene 3-(3',5'-di-tert-butyl-4'-hydroxyphenyl)propionate]methane) and 0.97% of a radiation cross-linking promoter (triallyl isocyanate), and then irradiating the adhesive coating to a dosage of 10 megarads.

The closure members used in this Example comprise uniaxially uniformly expanded sheets of cross-linked high density polyethylene, 45.7cm (18 inches) long. Table I below shows the modulus at 150°C, the expansion ratio and the thickness before expansion of each of the sheets. The sheets have a coating 1.52mm (60 mils) thick of a mastic on one surface thereof.

The substrate used in this Example consists of a steel pipe having a concrete lining 0.95cm (3/8 inch) thick. The pipe has an outer diameter of 8 inches and the thickness of the steel is 0.635cm (1/4 inch). Mounted concentrically on the centre of the pipe, is a steel collar 10.2cm (4 inches) long having an outer diameter of 35.6cm (14 inches). The closure member is wrapped around the substrate, with the mastic coating on the inside and with the collar in the middle of the sheet, and with an overlap of about 10.2cm (4 inches). The patch is then placed symmetrically over the exposed edge of the sheet and heated by means of a flame gun until the patch adhesive had reached its tack point and bonded the patch to the sheet; the patch is pressed against the sheet by hand using an insulated glove during the heating. The exposed surface of the remainder of the sheet is then heated to cause recovery thereof. Table I below shows the width of the patch and the slippage of the patch at the end of the procedure.

Further experiments under identical conditions except using a patch member 20.3cm (8 inches) wide show that under these circumstances, patch slippage is completely eliminated.

Further experiments under identical conditions except that the patch member is an 20.3cm (8 inches) wide glass-fibre reinforced sheet as disclosed in U.S. Patent No. 4,200,676 result in the sheet recovering in such a fashion that it slips out of contact with the patch, exposing the substrate.

TABLE I

Sheet No.	Thickness Before Expansion (mm)	Recovery Force (Kg.m ⁻¹)	Expansion Ratio	Modulus (Kg./m ⁻²)	Patch Slippage (mm)	Final Patch Width (cm)
1	1.12	16.4	1.47	24,300	1.6 - 6.3	17.1 - 17.8
2	1.09	21.8	1.67	25,400	3.2 - 12.5	16.1 - 19.7
3	1.09	28.6	2.00	24,900	6.3 - 22.2	19.1
4	1.09	30.7	2.08	25,400	3.2 - 9.5	17.8
5	1.50	44.9	2.0	27,000	6.3 - 31.8	17.1 - 21.6
6	1.52	46.3	2.04	28,100	4.8 - 12.5	19.7 - 21.6
7	1.52	59.2	2.56	26,900	6.3 - 28.6	20.3 - 21.6
8	1.55	76.0	3.33	25,200	6.3 - 22.2	21.0 - 22.5
9	2.08	69.7	3.23	17,800	6.3 - 25.4	20.3
10	2.08	87.8	3.85	18,600	6.3 - 19.0	21.6
11	2.08	88.3	4.00	17,900	6.3 - 19.0	22.2
12	2.08	105.0	4.76	17,800	3.2 - 9.5	21.3

Example 2

The procedure of Example 1 is followed except that (1) the sheet closure member was 30.5cm (12 inches) by 132.1cm (52 inches) and has an expansion ratio of about 1.3 and an M_{100} modulus at 150°C of 24,600 kg.m⁻² (35 psi), (2) the patch member is 15.24cm (6 inches) wide and 30.5cm (12 inches) long, (3) the pipe has an outer diameter of 40.6cm (16 inches) and the collar has an outer diameter of 45.7cm (18 inches), and the sheet when wrapped affords an overlap of about 7.6cm (3 inches). The patch stretches by about 15% in width and does not slip.

Example 3

The procedure of Example 2 is repeated except that the patch member is only 10.2cm (4 inches) wide. A similarly satisfactory result is obtained. However, use of a 10.2cm (4 inches) wide glass-fibre reinforced patch as described in U.S. Patent No. 4,200,676 results in failure, the sheet recovering to such an extent that it slips out of contact with the patch, exposing the substrate.

Example 4

The procedure of Example 2 is repeated with a series of pipes of varying diameter except that the patch member is only 5.1cm (2 inches) wide and the substrate is a pipe of uniform diameter 5.1, 15.2, 20.3, 35.6 or 122cm (2, 6, 8, 14 or 48 inches). A satisfactory result is obtained in all cases.

Example 5

The patch member of this Example is 3.8cm (1.5 inches) long and 10.2cm (4 inches) wide and consists of a 0.51mm (20 mil) thick sheet of cross-linked high density polyethylene having a modulus at 150°C of 59,800 kg.m⁻² (85 psi) and having adherent to one side thereof a 0.64mm (25 mil) thick layer of a cross-linked hot melt adhesive as described in Example 1.

The closure member is a uniformly expanded sheet of cross-linked high density polyethylene, 2.1mm (82 mil) thick and 3.8cm (1.5 inches) long, and having a modulus at 150°C of 17,600 kg.m⁻² (25) psi and an expansion ratio of 4.8:1. The sheet has a coating 1.52mm (60 mils) thick of a mastic on one surface thereof. The substrate is a steel pipe having an outer diameter of 10.2cm (4 inches) and a thickness of 0.76mm (30 mils). The closure member is wrapped around the substrate, with the mastic coating on the inside and with an overlap of about 10.2cm (4 inches). The patch is then placed symmetrically over the exposed edge of the overlapping portion sheet and heated by means of a flameless heat gun until the patch adhesive has reached its tack point and bonded the patch to the sheet; the patch is pressed against the sheet by hand using an insulated glove during the heating. The remainder of the sheet is then heated to cause recovery thereof. The ends of the sheet remain overlapping, with the patch covering the overlap area.

The procedure of Example 5 is followed except that the sheet closure member had no mastic coating in the overlap area. A similar satisfactory result is obtained.

Example 7

The patch member used in this Example is 4 inches long and 6.35cm (2.5 inches) wide and consists of a 0.64mm (25 mils) thick sheet of cross-linked high density polyethylene having a modulus at 150°C of $38,700 \text{ kg.m}^{-2}$ (55 psi) and having adherent thereto a layer 0.64mm (25 mils) thick of a cross-linked hot melt adhesive as described in Example 1. The closure members are uniformly expanded sheets of cross-linked high density polyethylene, 10.2cm (4 inches) long. Table II below shows the modulus at 150°C, the expansion ratio and the thickness before expansion of each of the sheets. All the sheets have a coating 1.52mm (60 mils) thick of a mastic on one surface thereof. The substrate consists of a solid aluminum cylinder having an outer diameter of 3.8cm (1.5 inches) and mounted concentrically on the centre of the cylinder, an aluminum collar 2.54cm (1 inch) long and having an outer diameter of 7.6cm (3 inches). The closure member is wrapped around the substrate, with the mastic coating on the inside and with the collar in the middle of the sheet, and with an overlap of about 15.2cm (6 inches). The patch is then placed symmetrically over the exposed edge of the over-lapping portion of the sheet and heated by means of a flameless heat gun until the adhesive

has reached its tack point and bonded the patch to the sheet; the patch is pressed against the sheet by hand using an insulated glove during the heating. The remainder of the sheet is then heated to cause recovery thereof. When using Sheet No. 4, the patch slips out of contact with the sheet, but in the other runs a satisfactory result is obtained.

TABLE II

Sheet No.	Thickness before expansion (mm)	Expansion Ratio	Modulus (kg.m ⁻²)	Recovery Force (Kg.m ⁻¹)
1	0.38	3	38,700	8.04
2	0.38	3	38,700	26.8
3	1.02	8	10,600	51.8
4	1.02	3	38.700	69.7

The values for tensile strength and elongation given in this specification and in the appended claims are measured by the method of ASTM D-638. The values for modulus at 150°C are measured by the following test, which measures the stress required to elongate the article by 100% at 150°C. Marks

separated by 2.54 cm (1 inch) are placed on the centre section of a die-cut specimen and the sample is hung vertically in an oven maintained at 150°C, with a 2 gm. weight attached to the lower end of the sample. After equilibrating for 2 minutes, the weight attached to the lower end of the sample is increased until the distance between the marks has increased by 100%. The modulus (also known as the M_{100} value) is then calculated from the expression

$$\text{Modulus} = \frac{\text{stress}}{\text{initial cross-sectional area}}$$

Lap shear is determined in accordance with the method of ASTM D-1002 with the modification that the thickness of the adhesive in the determination is equal to the thickness of adhesive to be used in the arrangement, and the further modification that the composition of the substrates used in the determination are the same as those of the patch member and the closure member of the arrangement of the invention.

The peel strength is determined by heat-recovering a sheet of polymeric materials to be used for the cover member about a drum of 25mm length and 25mm diameter so that the polymeric material covers, and is bonded to, the entire circumference of the drum. The surface of polymeric material is cleaned and degreased and a strip of the material to be used for the patch member approximately 50mm in length is wrapped around the drum with the layer of adhesive interposed between them, and the assembly is heated in an oven at 150°C for 20 minutes to bond the two materials together. The drum is then mounted with its axis horizontal so that it is

freely rotatable and the outer layer of material is peeled off in a radial direction at a rate of 50 ± 5 mm per minute at $23 \pm 2^{\circ}\text{C}$ using a suitable tensile test apparatus, the force required to peel the material being recorded as the peel strength.

CLAIMS:

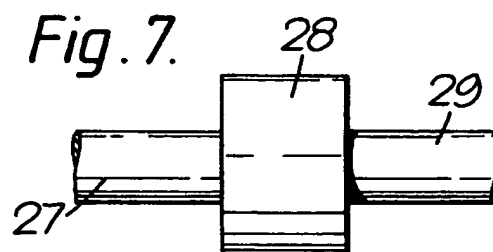
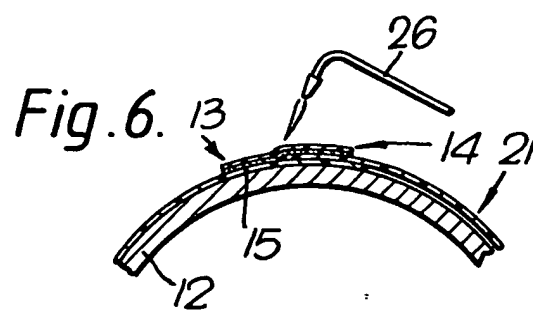
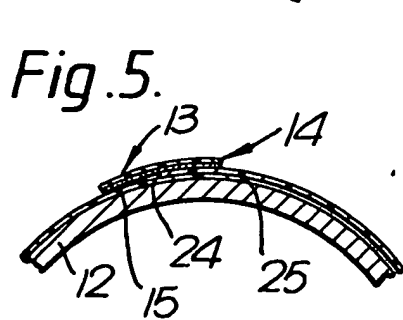
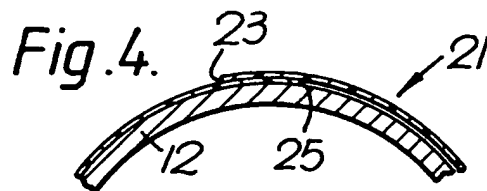
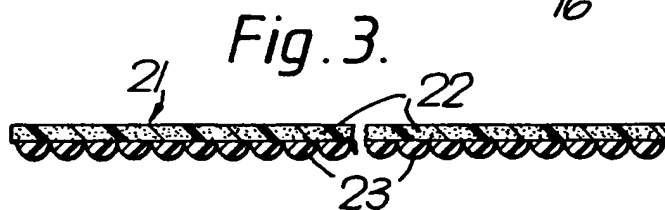
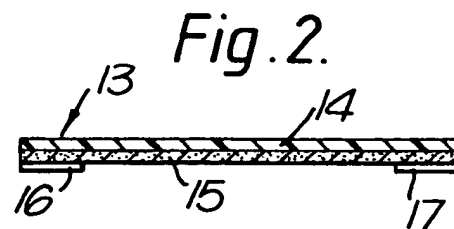
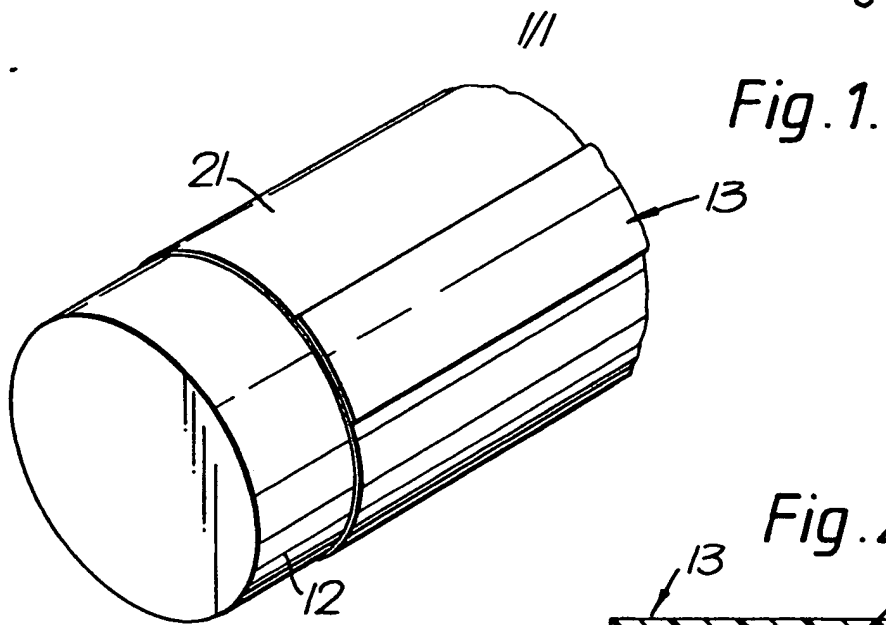
1. An arrangement for covering at least part of an elongate substrate (12) which comprises a heat-recoverable polymeric closure member (21) in sheet form adapted to be wrapped around the substrate so that one edge portion thereof overlies an opposite edge portion and recovered about the substrate by application of heat, a patch member (13) for retaining the edge portions together during recovery of the closure member, and a layer (15) of adhesive having a tack temperature below the recovery temperature of the closure member for securing the patch member to the closure member during recovery of the closure member, characterized in that the layer (15) of adhesive has a lap shear strength at 150°C of from 70 to 14,100 kg.m⁻² and the patch member (13) has a modulus at 150°C of from 1400 to 141,000 kg.m⁻² and an elongation at 150°C of from 10 to 1000%, the arrangement being such that when the closure member is heated, it will recover about the substrate and cause at least part of the patch member to stretch by at least 5% in the direction of recovery of the closure member.

2. An arrangement as claimed in claim 1 characterized in that the layer (15) of adhesive has a lap shear strength at 150°C of at from 700 to 8,500 kg.m⁻².

3. An arrangement as claimed in claim 1 or claim 2, characterized in that the adhesive has a melt viscosity at 150°C of at least 10² poise, preferably at least 10⁴ poise.

4. An arrangement as claimed in any one of claims 1 to 3, characterized in that the adhesive has a peel strength of at least 90 kg.m^{-1} .
5. An arrangement as claimed in any one of claims 1 to 4, characterized in that the patch member (13) has a modulus of from 35,000 to $106,000 \text{ kg.m}^{-2}$.
6. An arrangement as claimed in any one of claims 1 to 5, characterized in that the patch member (13) has an elongation at 150°C of from 50 to 200%.
7. An arrangement as claimed in any one of claims 1 to 6, characterized in that the patch member (13) comprises a cross-linked polymeric material.
8. An arrangement as claimed in any one of claims 1 to 7, characterized in that the product of the thickness of the patch member (13) and the modulus at 150°C of the patch member (13) is in the range of from 0.2 to 20 times the maximum recovery force (per unit length) of the closure member (21).
9. A method of covering at least part of an elongate substrate (12) which comprises wrapping a polymeric closure member (21) in sheet form around the substrate so that one edge portion of the closure member overlies an opposite edge of the closure member, heating a layer (15) of adhesive to its tack temperature and placing the layer of adhesive and a patch member (13) over the exposed edge (23) and outwardly disposed edge portions of the closure member so that the

layer of adhesive is interposed between the closure member and the patch member, pressing the patch member against the closure member to bond them together, and heating the closure member to cause it to recover into circumferential contact with the substrate, characterized in that the closure member (21), the layer (15) of adhesive and the patch member (13) together form an arrangement as claimed in any one of claims 1 to 8, and that the method is conducted under conditions such that the patch member remains bonded to the closure member over at least a major portion of its length and at least part of the patch member is stretched by at least 5% in the direction of recovery of the closure member.





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EUROPEAN SEARCH REP RT

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DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
D	<u>US - A - 3 770 556 (RAYCHEM CORP.)</u> * column 1, line 64 to column 2, line 36; column 3, line 58 to column 4, line 2; column 4, line 56 to column 5, line 3; fig. 5 * & DE - A - 2 139 445 ---	1,9	B 29 C 27/20 F 16 L 47/02
D,P	<u>US - A - 4 200 676 (RAYCHEM CORP.)</u> * column 2, lines 35 to 55; column 6, line 53 to column 7, line 25; fig. 1 to 6 * ---	9	TECHNICAL FIELDS SEARCHED (Int. Cl. 3)
A	<u>US - A - 3 959 352 (SIGMAFORM CORP.)</u> * column 2, lines 47 to 68; fig. 1 to 3 * & FR - A1 - 2 304 460 & DE - A1 - 2 611 518 ---		B 29 C 27/20 B 29 C 27/26 B 29 C 27/28 B 29 C 27/30 F 16 L 47/02 F 16 L 55/16 F 16 L 59/14
D	<u>US - A - 3 455 336 (RAYCHEM CORP.)</u> * fig. 1 * ---		CATEGORY OF CITED DOCUMENTS
D	<u>US - A - 3 379 218 (RAYCHEM CORP.)</u> * fig. 1 * ---		X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
<input checked="" type="checkbox"/> The present search report has been drawn up for all claims			&: member of the same patent family, corresponding document
Place of search Berlin		Date of completion of the search 31-10-1980	Examiner BRUCK